



Serbian Tribology Society



Faculty of Engineering
University of Kragujevac

SERBIATRIB '17

15th International Conference on Tribology

17 – 19 May 2017, Kragujevac, Serbia

PROCEEDINGS



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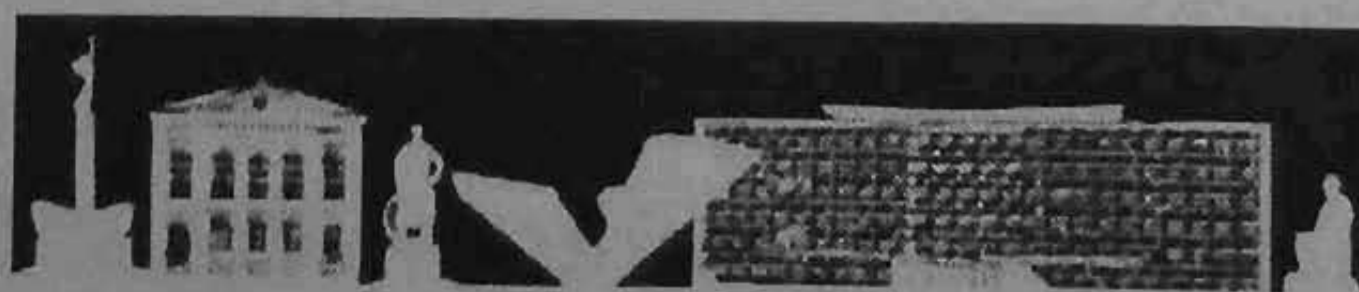
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EDITOR: Slobodan Mitrović



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METHODS AND PRINCIPLES OF DETERMINING THE FOOTWEAR AND FLOOR TRIBOLOGICAL CHARACTERISTICS

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Abstract: There are many standards relating to the anti-slip properties of footwear and flooring. These standards describe the different test methods and procedures for determining the footwear and floor slip resistance in different conditions. In this paper authors systematize the standards in this field applied in the EU and in Serbia and cite the Serbian institutes which are certified for this type of testing. In addition, the authors have carried out an analysis and comparison of the tests that are defined in these standards, indicating their advantages and disadvantages. Importance of the static and kinetic friction testing in determining the anti-slip properties of footwear and flooring is specifically indicated. Considering the current standards in area of slip resistance of the footwear and floor covering authors have determined the testing conditions for laboratory measuring the friction forces of different floor and footwear materials. The laboratory measurement has carried out at Faculty of Mechanical Engineering in Niš. The measuring results and their analysis are presented in the paper, as well.

Keywords: tribological characteristics, footwear, flooring, experimental methods, standards.

1. INTRODUCTION

Numerous accidents occur due to the slipping during human walking. Selection of appropriate shoes and floor combination, considering the slip resistance properties, is the most important measure for slipping accidents prevention. Evaluation of floor and footwear slip resistance should be based on understanding of basic tribological characteristics. There are different principles and methods to assess the slip resistance of flooring coverings and footwear.

Wetzel et al. [1] describe the requirements concerning the slip resistance and the state of slip resistance measurement standards in the European Union. They note: "Slip resistance is influenced by a numerous factors, such as:

combination of shoe sole, floor covering, contaminants and their properties; surface structures of shoe soles and floor coverings and changes to them as a result of wear; motion speed and ambient parameters" [1].

The comparison of the slip resistance of outdoor footwear and safety footwear according the performed experimental research is described in the paper [2].

In paper [3] author points out that there are many different standards and methods for assess the slip resistance, but there are no obligation to apply them for the producers of footwear and floors. He indicates that evaluation of slip resistance should be based on understanding of basic tribological characteristics between the shoes and floors.

A number of organizations have developed standard tests for measuring friction force i.e. coefficient of friction. These tests have numerous similarities, but vary greatly in type and purpose. List of tests that have been standardized by ASTM is presented in [4]. Some are directed towards a particular application, while others are for general evaluation of materials.

Structural, operation and interaction parameters should be taken into account in friction experimental research of solid elements [5]. The contact between rubber and hard material is specific compared to pure metal-metal contact. In contact between rubber and hard surface, friction depends significantly on load and on geometry of the surfaces [6]. The author in the paper [7] claims that friction force between rubber and rough (hard) surface can be described by the adhesion and hysteretic components.

There are different European standards that have adopted various test methods and rating systems [11-15]. These standards include test methods that are based on different principles and are used under different conditions. Analysis of their advantages and disadvantages are presented in papers [8-9].

Basic factors influencing accidents and injuries in human walking can be divided in next groups: footwear, floor, human factors and environment (location) [10]. Footwear factors are: sole construction, sole material, sole elasticity, sole hardness, tread pattern, wear etc. Floor factors are: material type, roughness, hardness, maintenance, wear, etc. Human factors represent individual characteristics of human such as gait, age, weight, mobility, etc. Environment factors are lighting, humidity, obstacles, changes of surfaces, contaminants, etc.

Footwear and floor factors in friction testing are considered in this paper.

2. BASIC PRINCIPLES OF FRICTION TEST METHODS

The basic principle of determining the footwear and floor slip resistance is testing the

real materials in real conditions considering the tribological characteristics.

The possibility of determination of friction coefficient is presented on Figure 1.

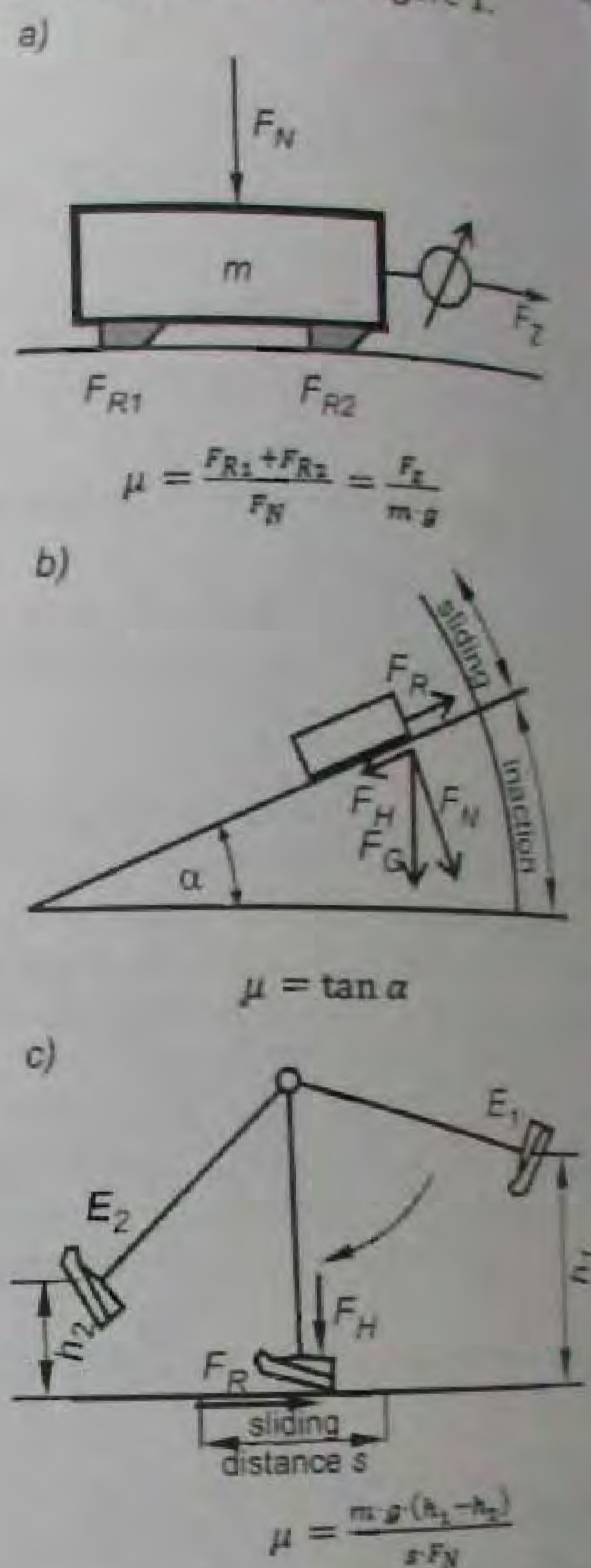


Figure 1. Friction coefficient determination by pulling force (a), friction angle (b) and energy loss (c)

Main principles of friction coefficient determination are the tests with measuring of the pulling force (Fig. 1a), where friction coefficient is ratio of pulling force (F_z) and pulled weight (mg); tests with measuring the friction angle (Fig. 1b), where friction coefficient is in function of friction angle (α); and tests with measuring of energy loss due to friction (Fig. 1c), where friction coefficient is a function of difference of potential energies ($E_1 - E_2$) - potential energy at the start, E_2 - potential energy at the end of measurement).

2.1 Static and dynamic coefficient

There are static and dynamic friction force and according to opposing views about the importance of static and dynamic coefficient of friction measurement. Some engineers consider dynamic coefficient of friction more important than the static coefficient of friction in the evaluation of slip resistance.

The static coefficient of friction is greater than the dynamic coefficient of friction and it is the initial barrier against slippage. Once slippage has begun, a lower coefficient of friction may be maintained.

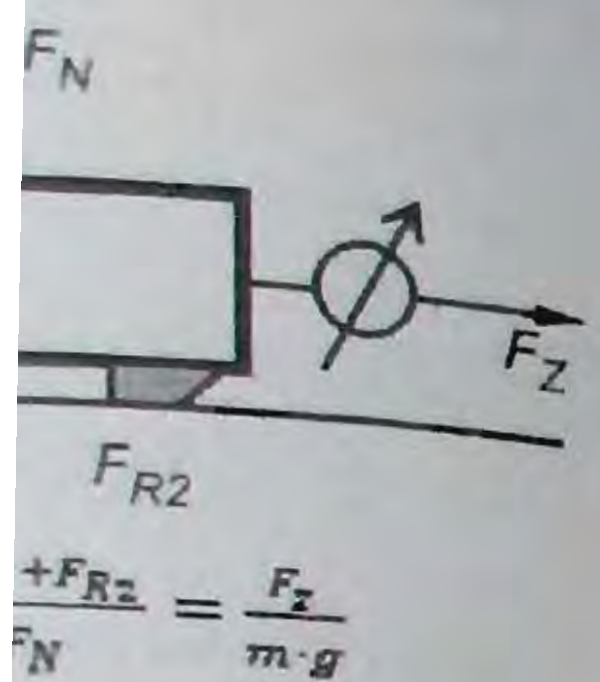
Static friction is friction between two bodies that are not moving relative to each other. The static friction force is overcome by an applied force before any motion occurs. The static friction has an important role in transport means, especially in road vehicles, but also in many other applications. Regardless of the installed power units, motion of a vehicle is possible only if there is an adequate static friction between the drive wheels and the ground. The static friction between shoe soles and floor coverings is necessary for human walking.

2.2 Basic group of parameters for friction test

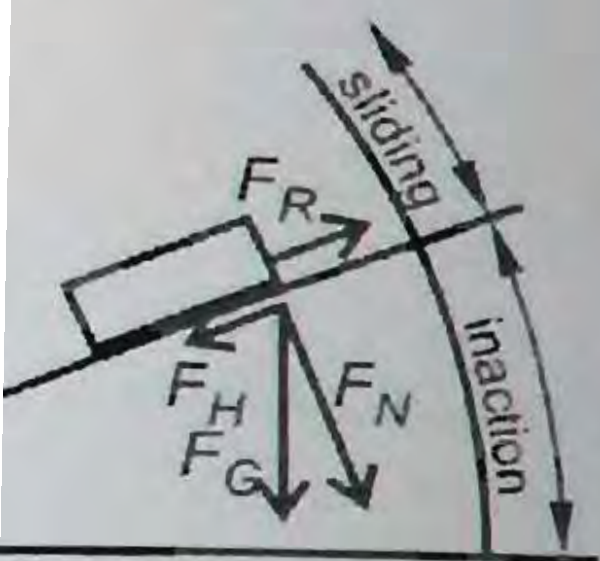
In a friction test the required tribological characteristics data must be determined for the tribological systems characterized by the following group of parameters:

- **Structural parameters** - characterize the tribological system (materials, lubricants, surface roughness, etc.) involved in the friction process and their physical, technological properties.
- **Operational parameters** - loading, kinematic conditions and duration.

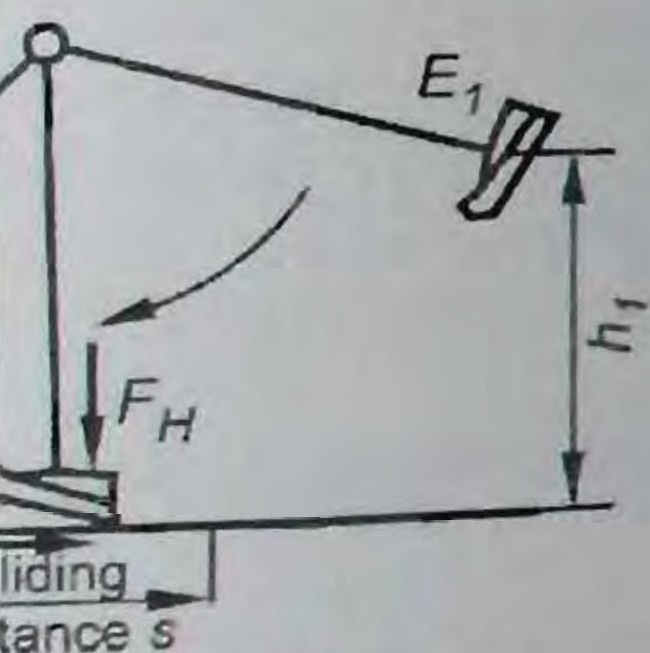
al conditions considering characteristics. determination of friction ed on Figure 1.



$$\frac{F_{R2}}{F_N} = \frac{F_z}{m \cdot g}$$



$$\mu = \tan \alpha$$



$$\mu = \frac{m \cdot g \cdot (h_1 - h_2)}{s \cdot F_N}$$

coefficient determination by friction angle (b) and energy loss (c)

s of friction coefficient the tests with measuring of (Fig. 1a), where friction of pulling force (F_z) and tests with measuring the (Fig. 1b), where friction of friction angle (α); measuring of energy loss due to where friction coefficient is a ce of potential energies (E_1 at the start, E_2 - potential f measurement).

static and dynamic coefficient of friction

There are static and dynamic (kinematic) friction force and according to that static and dynamic coefficient of friction. There are opposing views about the importance of static and dynamic coefficient of friction in slip measurement. Some engineers claim that the dynamic coefficient of friction is more important than the static coefficient for an evaluation of slip resistance.

The static coefficient of friction is usually greater than the dynamic coefficient of friction and it is the initial barrier against slippage. If slippage has begun, a higher dynamic coefficient of friction may help one to recover from a slip, but it is better to prevent the slippage and static friction is relevant for that.

Static friction is friction between two bodies that are not moving relative to each other. The static friction force must be exceeded by an applied force before an object can move. The static friction has an important role in transport means, especially in railway and road vehicles, but also in human walking. Regardless of the installed power of the drive units, motion of a vehicle is only possible if there is an adequate static friction between the wheels and the ground. In the same way static friction between shoes sole and floor coverings is necessary for human motion.

Basic group of parameters in a friction test

In a friction test the resulting tribometric characteristics data must be understood as tribological systems characteristics associated with the following group of parameters [5]:

- **Structural parameters**, which characterize the components (materials, lubricant, and environment) involved in the friction process and their physical, chemical, and technological properties;
- **Operational parameters**, that is, the loading, kinematic, and temperature conditions and their functional duration;

- **Interaction parameters**, which characterize, in particular, the action of the operating parameters on the structural components of the tribological system and define its contact and lubrication modes.

Structural parameters include triboelements, interfacial element such as lubricant or dirt particles, and environmental medium such as air or moisture. Structural parameters can be divided in:

- Geometric parameters (geometry dimensions, surface topography, etc);
- Microstructural parameters (grain size, dislocation density, etc);
- Mechanical parameters (elastic modulus, hardness of triboelements; viscosity and viscosity-pressure of interfacial elements and environmental medium, etc)
- Chemical parameters (volume composition and surface composition of triboelements; composition of interfacial elements and environmental medium such as acidity and humidity, etc)
- Physical parameters (density, thermal conductivity, etc).

The basic operational parameters in tribology [5] are:

- Type of motion (sliding, rolling, spin, and impact; the kinematics can be continuous, intermittent, reverse, or oscillating);
- Load, defined as the total force (including weight) that acts perpendicular to the contact area between triboelements;
- Velocity, to be specified with respect to the vector components and the absolute values of the individual motions of triboelements;
- Temperature of the structural components at stated location and time, that is, the initial (steady state) temperature and the friction-induced temperature rise;

- Time dependence of the set of operational parameters;
- Duration of operation or test.

2.3 Friction conditions in contact rubber-substrate

Rubber is the most often used material for shoe sole, so the contact between rubber and hard material should be studied. Rubber friction differs in many ways from frictional properties of most other solids due to very low elastic modulus of rubber and high internal friction.

In situation of contact between rubber and hard surface the friction depends markedly on load and on geometry of the surfaces [6]. Rubber is a truly elastic solid and if the sliding surfaces are flat (so that they touch over a large number of contact regions) the area of contact and friction force are more nearly directly proportional to the load.

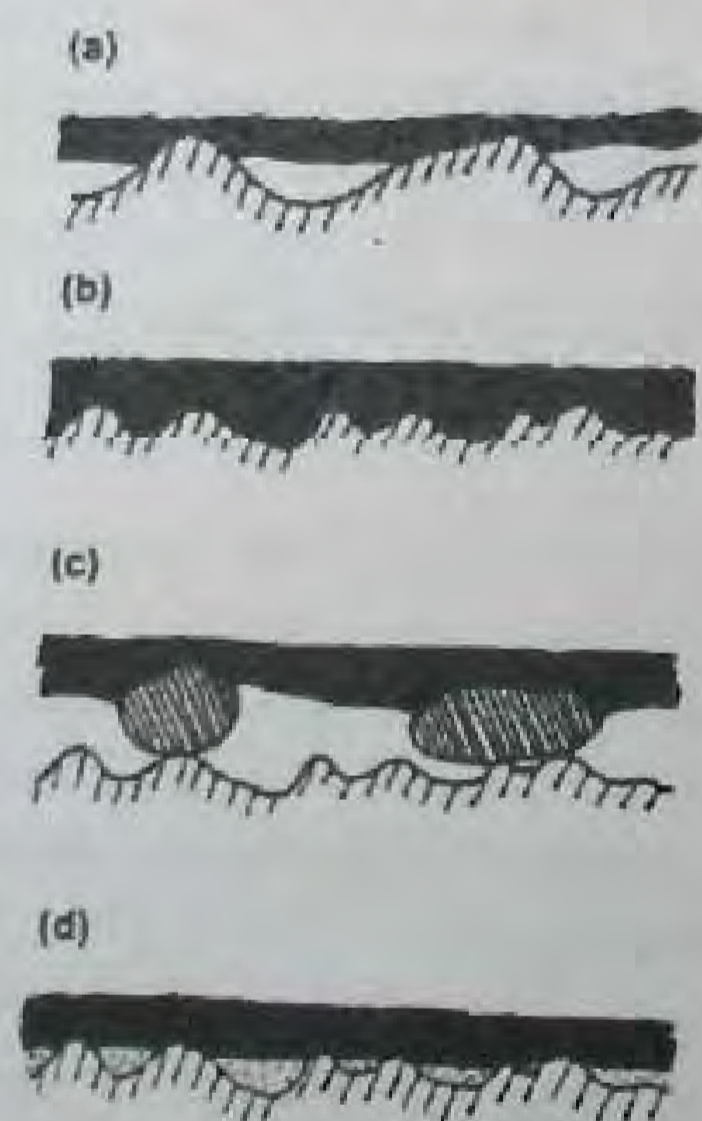


Figure 2. Rubber in contact with a hard substrate with a rough surface [7]

When a hard steel ball slides over a clean rubber surface the friction is dominated by the adhesion between the surfaces. When the surfaces are thoroughly lubricated the friction is dominated by the deformation of the rubber due to elastic hysteresis losses [6].

The friction force between rubber and rough (hard) surface can be described by the adhesion and hysteretic components [7].

Contact of rubber and hard substrate with a rough surface is presented in Figure 2 in different conditions [7]. Rubber on a hard substrate with long-wavelength surface roughness is shown in Figure 2a. Because of adhesion to the substrate, rubber in contact area deforms in to completely follow the short-wavelength surface roughness profile of the substrate (Figure 2b). Rubber surface dusted by small particles sliding on a hard substrate is presented in Fig. 2c and rubber sliding on a water covered surface is presented in Figure 2d.

3. FOOTWEAR AND FLOOR SLIP RESISTANCE STANDARDS

Testing and assessment of anti-slip characteristics of footwear and floor is of major importance for the prevention of slipping accidents. Numerous different methods and devices have been developed over the years to measure the slip resistance of floor and footwear. Different European countries have adopted various test methods and rating systems. Because these test methods are based on different principles and are used under different conditions there is no correlation between them. No single test currently in use is perfect. All have their advantages, but also their own particular disadvantages [8].

The most often used standard tests for floor testing are Ramp test according to the German norms DIN 51130 and DIN 51097, Pendulum test according to the British and EU norm BS EN 13036-4, and tribometer test according to the norms DIN 51131 and BS EN 13893. The operating principle of ramp test is measuring of the friction angle; the principle of pendulum test is measuring the energy loses due to the friction and the tribometer test is based on measuring the pulling force which is actually the friction force.

In the ramp test (DIN 51130), a test person (operator) is wearing standard footwear and walks backwards and forwards over a sample of a flooring material that has been evenly coated with oil (Figure 3). The angle of the

ramp is increased until the test person slips. The acceptance angle α is used to express the degree of slip resistance of the barefoot.



Figure 3. Ra

According to the angle of the slip resistance that

Table 1. Slip resistance according to the norm DIN 51

Classification	R 9	R 10
Slip angle [°]	6÷10	10÷19

The pendulum test measures the energy due to friction as the slider assembly slides over the surface [12]. Pendulum test is presented in Figure 4. The standardized value of slip resistance is the pendulum test value (P)



Figure 4. Pendulum

hard substrate with
 Figure 2 in
 Rubber on a hard
 wavelength surface
 Figure 2a. Because of
 e, rubber in contact
 completely follow the
 roughness profile of
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 es sliding on a hard
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OR SLIP RESISTANCE

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 and tribometer test
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 at has been evenly
). The angle of the

is increased until the operator slips [11].
 the acceptance angle obtained is used to
 express the degree of slip resistance. In the
 ramp test (DIN 51097) the operator walks
 on a ramp.



Figure 3. Ramp test

According the angle of ramp there are five
 classes of slip resistance that is shown in Table 1.

Table 1. Slip resistance classes of floorings
 according to the norm DIN 51130

Classification	R 9	R 10	R 11	R 12	R 13
Slip angle [α]	6÷10	10÷19	19÷27	27÷35	>35

The pendulum test measures the loss of
 energy due to friction as the standard rubber-
 coated slider assembly slides across the test
 surface [12]. Pendulum friction tester is
 presented in Figure 4. It provides a
 standardized value of slip resistance. This is
 the pendulum test value (PTV).



Figure 4. Pendulum friction tester

The pendulum is the preferred test method
 in the United Kingdom. Relative risk of slipping
 is determined with PTVs (Table 2).

Table 2. Slip potential due to PTV

Slip potential	PTV
HIGH	0÷24
MODERATE	25÷35
LOW	>36

Tribometer test method is based upon a
 friction force measurement. A body equipped
 with sliders is pulled at a constant speed over
 the flooring surface. The force required to pull
 the body is determined over the length of the
 measuring distance. An example of a
 tribometer tester according to the norms DIN
 51131 is shown in Figure 5.



Figure 5. An example of a tribometer tester



Figure 6. Test equipment for measurement the slip
 resistance of footwear

In order to determine the sliding friction
 coefficient, this force is divided by the
 vertically acting force. This test can be carried
 out in wet and in dry conditions both in a
 laboratory and on-site. This device is
 predominantly used in Germany, Poland and
 Austria [9].

The method for measurement of the slip resistance of shoes is described in EN 13287 [14]. The footwear to be tested is placed on the base of ceramic tile or steel floor, subjected to a given normal force (Figure 6). The base is moved horizontally and sliding of footwear occurs.

Dynamic coefficient of friction is calculated according the measured frictional force. Glycerin or sodium lauryl sulphate solution acts as contaminant on the surface.

Some EU standards related with measuring of slip resistance of footwear and floor coverings are adopted in Serbia. There are:

SRPS EN ISO 13287:2014 - Personal protective equipment - Footwear - Test method for slip resistance;

SRPS EN 13036-4:2012 - Road and airfield surface characteristics - Test methods - Part 4: Method for measurement of slip/skid resistance of a surface: The pendulum test;

SRPS EN 13893:2011 - Resilient, laminate and textile floor coverings - Measurement of dynamic coefficient of friction on dry floor surfaces.

Manufacturers and distributors of protective footwear in Serbia are usually required to test their products according to standard SRPS EN ISO 13287. But manufacturers and distributors of other types of footwear rarely present the slip resistance properties of their products. In rare cases they advertise the slip resistance of their shoes referring to standards EN ISO 13287 and DIN 51130.

Manufacturers and distributors of sports flooring in Serbia presenting their products usually refer to standard EN 13036-4 (Pendulum test). Manufacturers and distributors of laminate and textile floor coverings most often refer to standard EN 13893. Other manufacturers and distributors of floor coverings refer to standard DIN 51131, DIN 51130 and DIN 51097.

4. EXPERIMENTAL INVESTIGATION

Determination of floor and footwear slip resistance is often conducted by measuring

the friction force and calculating the coefficient of friction. Dynamic (kinetic) coefficient of friction is the most often determined.

The requirements setting in the standard very often are not in compliance to the real conditions. For example in standard DIN 51130 specimens of floor material is the same material as the application, but footwear is special, and walking of test person is with low speed. Also, this way of walking on ramp isn't the same as walking on horizontal surface. In pendulum test sliders are made of materials with specific characteristics which are not similar to the shoe sole. The kinematic of pendulum isn't similar with kinematic of human walking/running, as well.

The contact pressure depends on the person's weight and surface texture and shoe soles, and the relief (texture) of substrate. Velocity of sliding corresponding to human stroke has a great range, from slow walking to running.

Importance of dynamic and static coefficient of friction should be considered as the equal.

Based on the above, in experimental determination of friction coefficient it is significant to provide the following:

- Experimental samples should be made of real shoes sole/floor materials with determined mechanical properties,
- Surface structure (macro and micro structure, roughness, etc.),
- Contact pressure,
- Sliding velocity,
- Contact condition (temperature of contact bodies, lubricant, contaminants, etc.),
- Environment (temperature, humidity, etc).

In order to estimate the laboratory test procedure and check the test conditions experimental research is performed at Faculty of Mechanical Engineering in Nis, Serbia.

Principle of determining the friction coefficient in performed experimental research is measuring the pulling force. Applied measuring method is based on settings in standards EN 13893 and DIN 51131. The measurement was carried out on dry and

wet surfaces. The test facility is equipped with sliders which are pulled parallel to the floor covering.

Materials of sliders were shoe sole, rubber and leather (three pieces, dimensions 10x40 mm) cut from real shoes. Experimental samples of floor coverings were three different materials: ceramic tiles and linoleum (vinyl). Contact pressure was 91 kPa.

Sliding distance was 500-800 mm. Sliding velocities were: 2, 10, 50 and 250 mm/s.

Friction force was measured and dynamic coefficient of friction was calculated in experimental research.

The test equipment is shown in Figure 7.



Figure 7. Test equipment in laboratory of mechanical engineering in Nis.

A typical example of measured force is presented in Figure 8.

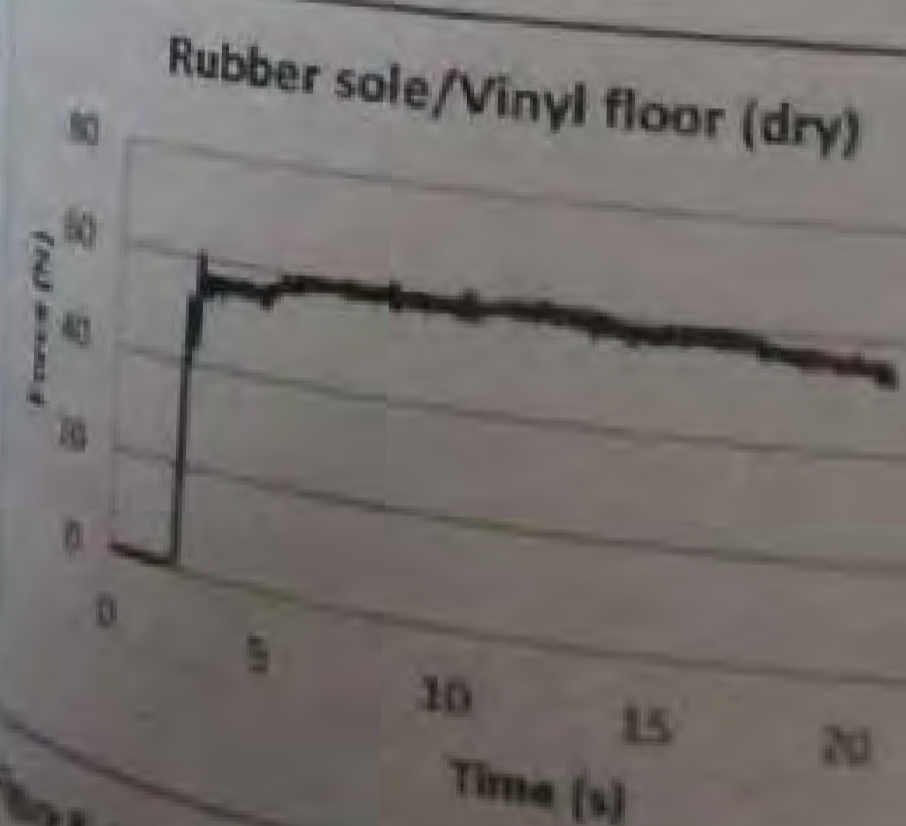


Figure 8. Measured friction force in sliding test sample on vinyl floor covering. The graph shows that the static and kinetic coefficients of friction are very similar, with only minor differences between static and kinetic values in dry conditions.

and calculating the dynamic (kinetic) friction coefficient is the most often

setting in the standard compliance to the real material is the same material, but footwear is of test person is with low of walking on ramp isn't on horizontal surface. In are made of materials characteristics which are not sole. The kinematic of similar with kinematic of ng, as well.

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(temperature of contact contaminants, etc.), perature, humidity, etc). hate the laboratory test ck the test conditions h is performed at Faculty ering in Nis, Serbia.

termining the friction rformed experimental ng the pulling force. method is based on EN 13893 and DIN 51131. s carried out on dry and

surfaces. The test facility is equipped with rollers which are pulled parallel to the surface of floor covering.

Materials of sliders were shoe sole made of rubber and leather (three pieces with dimensions 10x40 mm) cut from the real experimental samples of flooring covers of three different materials: laminate, ceramic tiles and linoleum (vinyl). Contact pressure was 91 kPa.

Sliding distance was 500-800 mm. Sliding velocity were: 2, 10, 50 and 250 mm/s.

Friction force was measured and coefficient of friction was calculated in experimental

equipment is shown in Figure 7.

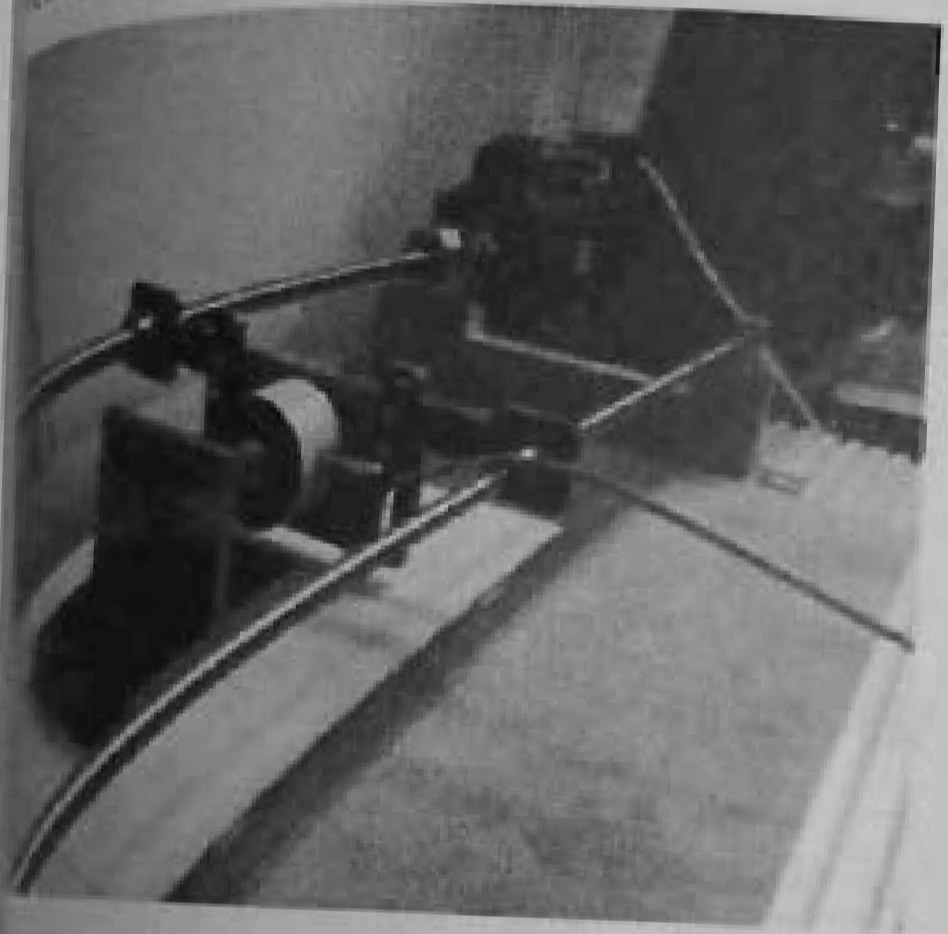


Figure 7. Test equipment in laboratory at Faculty of mechanical engineering in Nis

Figure 8. Typical example of measured friction force presented in Figure 8.

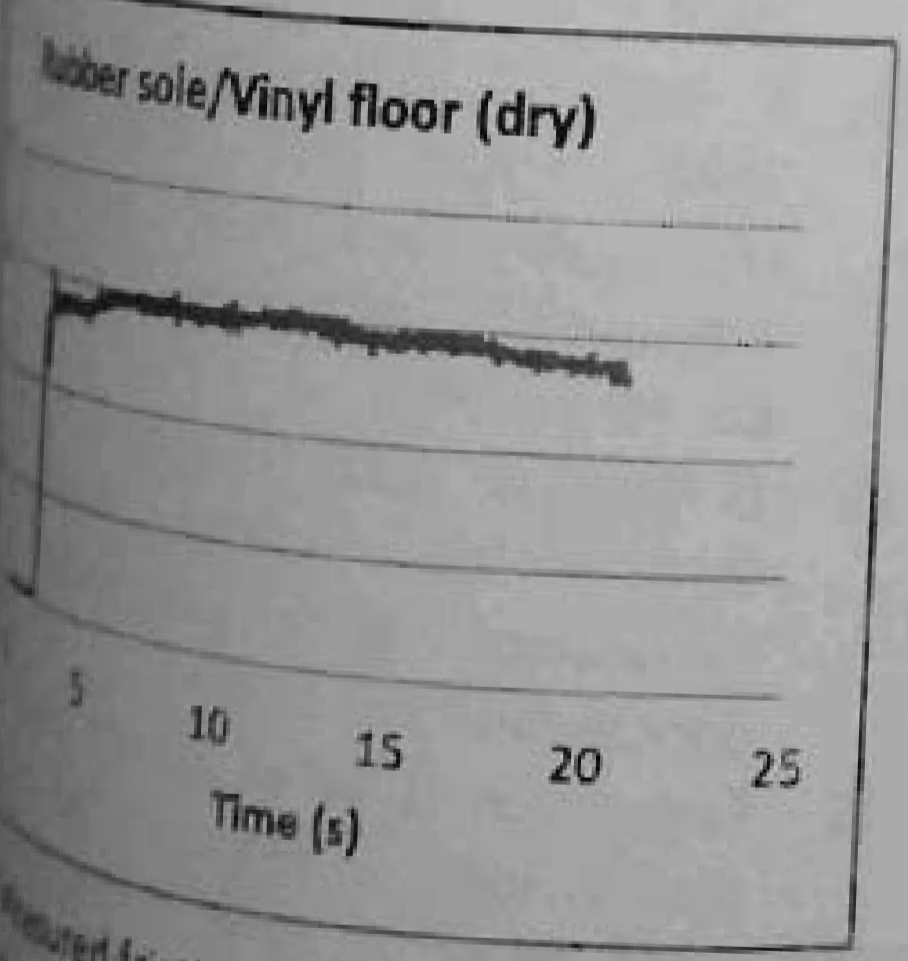


Figure 8. Measured friction force in sliding rubber sole on vinyl floor covering

Static and kinetic coefficients of friction were measured during the experiment. There are differences between static and kinetic coefficient values in different

type of contact and different conditions (Figure 9). Static and kinetic friction coefficient values presented in Figure 9 are average values of groups which consist of five measurements.

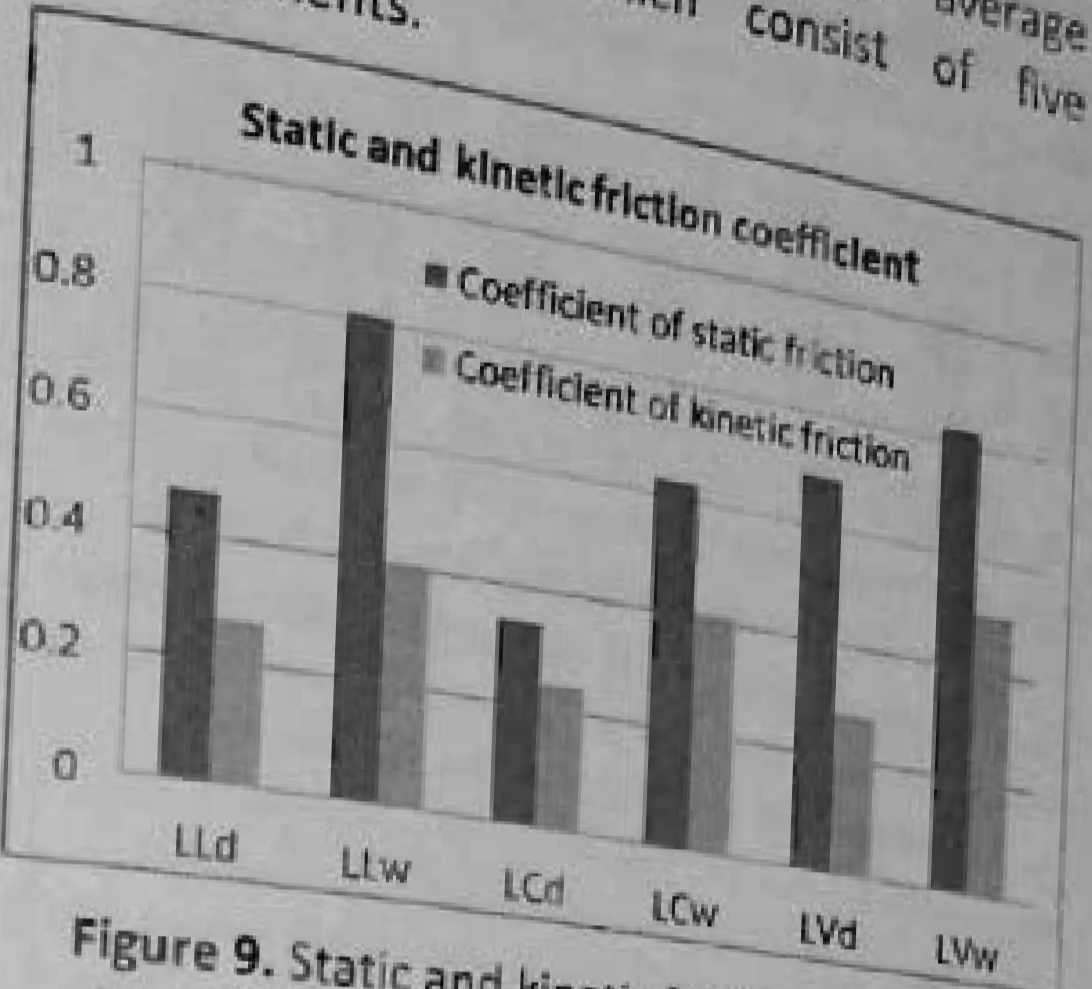


Figure 9. Static and kinetic friction coefficient values (LL-leather-laminate; LC-leather-ceramic tile; LV-leather-vinyl; d-dry contact; w-wet contact)

In most cases the values of static friction coefficient is higher than kinetic friction coefficient. But in some situations static friction coefficient is equal or smaller than kinetic friction coefficient.

Investigation of different contact conditions and different material samples required numerous tests (measurements). Each contact case was tested five times. Deviations of friction coefficient values within the group of measurement were not so big. Figure 10 presents the maximum and minimum values of friction coefficients in testing the leader sole samples on floor coverings within the twelve groups of five measurements.

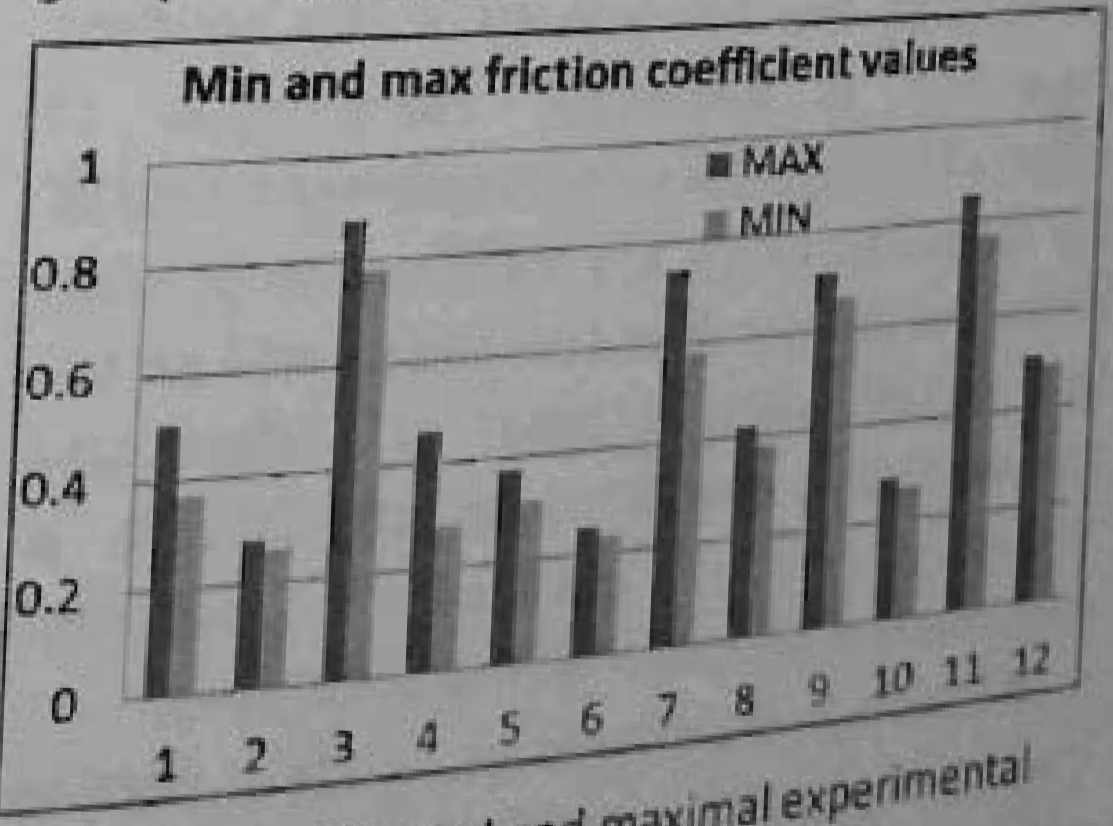


Figure 10. Minimal and maximal experimental friction coefficient values

Comparing the kinetic friction coefficient values in dry and wet condition it can be seen that values in wet condition are bigger in case

of leather sole sliding on all types of flooring coverings (Figure 11).

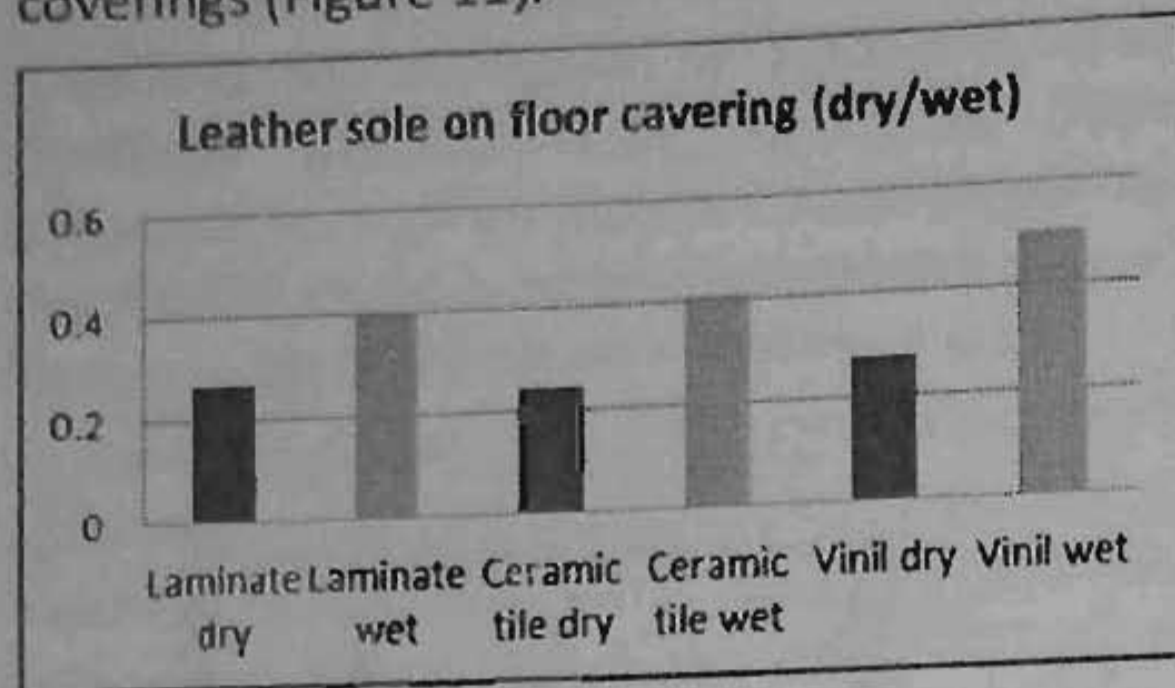


Figure 11. Average values of kinetic friction coefficient values in case of leather sole samples

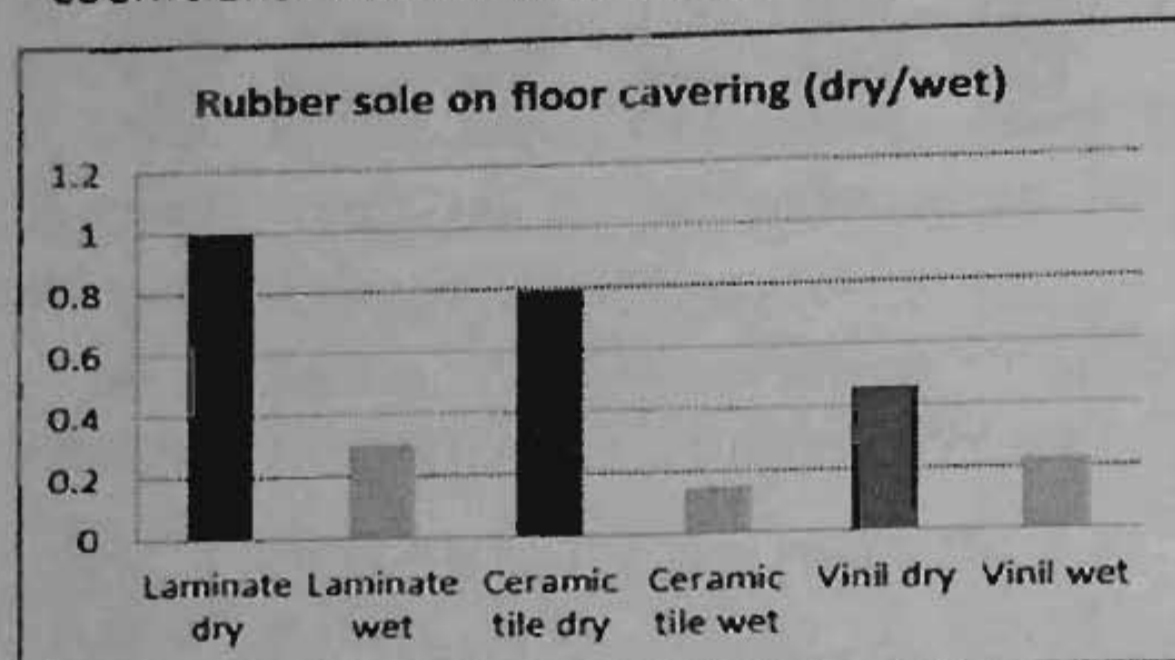


Figure 12. Average values of kinetic friction coefficient values in case of rubber sole samples

In contrast to the case of leather sole samples, kinetic coefficient of friction in case rubber sole sliding is two to three times lower in wet condition than for the dry condition (Figure 12).

5. CONCLUSION

There are numerous causes of slip accident in human walking and they are mostly stochastic. The key activity in slip accident prevention is systematic examination of influential parameters and implementation of the measures which are sufficient to prevent harm. But no one shoe sole design will be the best on all different types of surface and contaminants, and because of that it is necessary to investigate different combinations of materials and conditions.

Measuring (determining) of the friction coefficient should be conducted in conditions which are identical with real conditions. Measuring with different types of shoe sole (soft and hard; smooth and rough) should be conducted in cases where the substrate

material is known. In order to provide environmental conditions that may occur in real conditions (sunny, very hot, cool, dry, wet, rain, wet-snow, etc.) on-site testing is preferably. If shoe material is known, flooring materials should vary with different properties of hardness, macro and micro texture, etc.

Evaluation of floor and footwear slip resistance should be based on recognition of the basic tribological parameters and their testing.

Assessment of the floor and shoe slip resistance should be based on the recognition of the basic tribological parameters for specific friction contact and their testing in application conditions.

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A GRAPHIC ANALYTICAL MODELING LINEAR CONTACT BETWEEN STEEL AND COMPOSITE MATERIALS REINFORCED WITH GLASS FIBERS AT HIGH PRESSURES AND TEMPERATURES

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Abstract: Issues of wear occur in the thermoplastic injection molds at high temperature and high speed injection so they can achieve a pressure of 100 MPa and temperatures of 210 °C Steels used have been C120 which is used to make steel screws injectors and Rp 3 is a tool steel. In this article we are showing a graphical analytical modeling linear contact, between steel and composite materials reinforced with glass fibers (SGF) at high pressures and high temperatures, based on experimental determinations of the worn surface depending on the metal friction coefficient and the evolution of the temperature. The purpose is the evaluation of the dependence of the sliding speed and the load loading of the specimen, the amount of wear evaluated and measured depth of wear. The thermoplastic composite material transfer processes due to metal abrasion and corrosion, adhesion to the contact determined with Archard relationship by measuring the length of all using three points were determined graphically. A wear volume and depth of wear depending on load and contact pressure for different composite materials reinforced with glass fiber.

Keywords: contact temperature, friction coefficient, plastic material transfer, hardness of steel, steel surface wear, plastics with glass fibers, dry friction, linear contact.

1. INTRODUCTION

The process of injecting thermoplastic materials for injection molding machines with auger is highly complex, including numerous factors which influence the wear of metal surfaces in permanent contact with the material at melting temperature. In the technical literature, the following wear factors for injection molding machines are known: the processing conditions (auger geometry, working temperature, working pressure), the steels used for fabricating the cylinder and the auger, the geometrical conditions between the cylinder and the auger.

In the injection process two conditions must be observed: the composite materials have different lubrication properties in molten state which, if not strictly observed, lead to an interruption of material feed in the cylinder and therefore to the increase of adhesion wear. The second condition for the process of filling the cylinder is that there should be no areas with molten material present or areas with partially molten material, as they will lead directly to an increase in the wear of metal surfaces coming into contact with the injected material.

Composite materials containing corrosive volatile elements are a special case. These

evaporate in the cylinder during the injection process and thus lead to a corrosive wear. Composite materials reinforced with glass fibers have different mechanical properties within the cylinder. The friction coefficient values for the friction coefficient was presented with micro wear occurring via contact. Bilik values for the friction coefficient constant, observing that the value of the temperature, the state of the contact pressure. Dwyer used elastic, hydraulic and tests. Using the spherical method studying the removal of partially sliding contact with Stachowiak, et al. [3] have experimental testing pin-on-abrasive particles and ball-on-abrasion study three-body abrasion. He found that the best direct correlation between the amount of wear and particles is present in the case. Li, et al., [4] studied the mechanical properties by hardness tests. Using SEM (scanning electron microscope) scanning, Charalambous studied the temperature dependence of the wear mechanism at molten state. Myshkin [6] studies the deformation of materials and the adhesion between materials and notices that the friction force is much higher than the adhesive component. For adhesion known Johnson-Kendall-Roberts theory [7] and the Derjaguin-Muller-Boersma theory [8]. Shen and his colleagues have studied the wear behavior of high molecular-weight polyethylene and of the Delrin polymer. They established a relationship between the wear volume, normal pressure, and sliding distance. Chang and Friedrich [10] have shown that nanoparticles improve the properties of short fiber reinforced polymers.



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